Ozonolysis in Flow using the Vapourtec System

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Introduction Ozone is an oxidant that has been used for decades in organic synthesis and in the purification/deodorisation of water.¹ Ozonolysis is the addition of ozone to a substance resulting initially in a primary ozonide (molozonide) which then usually rearranges to a more stable secondary ozonide (trioxolane) in the case of alkenes (Scheme 1). Scheme 1 Reactant/ Solvent Pump **Reductive Workup:**ketones (R = alkyl, aryl) Pump Quench aldehydes (R & $R^3 = H$, $R^1 \& R^2 = alkyl, aryl)$ ◄— **Oxidative Workup:-**Above is a schematic showing the apparatus used in this work. The Vapourtec R4 acids (R & $R^3 = H, R$ trioxolane is connected to an ozoniser and ozone analyser. The Vapourtec cooled reactor module was & R^2 =alkyl, aryl) used to attain the low temperatures required to control the exothermic reaction. Three fourway valves were used to enable the location of the ozone analyser to be "hot switched" This transformation has great utility in synthesis both in a research and an from before to after the reactor module. industrial setting. The advantage of using ozone followed by reductive workup over other oxidants is the low cost and toxicity of the by-products i.e. DMSO from DMS, Ph₃PO Chemistry from PPh₃ as compared with high oxidation level metallic oxidants e.g. Chromium. Some of the drawbacks of using ozone at scale are the high exotherms associated with the initial reaction of substrates with ozone. Also the intermediate ozonides are unstable (although Initial studies were carried out using the aliphatic alkene 1-decene 1 and some can be isolated at room temperature) and are an explosion risk due to the weak O-O triethylphosphite as the reductive quench reagent (Scheme 2, Table 1). single bond. Thus, the build up of these materials must be avoided. The use of continuous Scheme 2 flow can alleviate both the exotherm problem and the build up of potentially explosive materials (if suitable reagents are used to quench them in flow). 1. O₃/O₂, -10 °C 2. (EtO)₃P, -10 °C <u>Setup</u> EtOAc Table 1 Cartridge O_2/O_3^1 EtO₃P Decene Entrv (ml/min) (**ml**) 0.25 (1.5) 0.25(1.0)25 (2.4) 10 25 (1.2) 0.50(1.5)10 0.25 (1.5) 25 (1.2) 10 0.25 (1.5) 25 (2.2) 0.25(1.0)0.25(1.5)0.25(1.0)25(1.5)0.25 (1.0) 0.25 (1.5) 25 (1.5) 0.07 1. Equivalents shown in brackets; 2. GC ratios; * Decene 0.4 M, (EtO)₃P 0.6 M. Successful conversion of 1-decene to products with as little as 1.2 eq. of O_3 and a small reactor cartridge (volume = 0.07 ml) was achieved. Unfortunately the selectivity for the aldehyde was poor and after further studies it was found that the intermediate The Vapourtec R4 system is a widely established piece of equipment in an trioxolane was being inefficiently reduced to the desired aldehyde 2. It was concluded that industrial R & D setting and has many uses in liquid-liquid systems. Most R & D centres triethylphosphite was unable to reduce the ozonides cleanly within the short reaction times also have access to an ozoniser. The coupling of these relatively common pieces of seen in the flow reactor. equipment gives many advantages over a purpose built system; these are modularity, cost, versatility and simplicity.





References

Bailey, P. S., Ozonation in Organic Chemistry, Vol 1. Olefinic Compounds, 1978; Vol 2. Nonolefinic Compounds, Academic Press, New York, 1982.



$3C$
 \bigcirc_{7}^{O} 2
 OH 3
 3C \bigcirc_{7}^{OH} 3

onanal ²	Nonanoic Acid ²	Decene ²
1.0	0.50	ND
1.0	0.40	0.2
1.0	0.50	ND
1.0	0.50	ND
1.0	0.42	ND
1.0	0.34	ND

Table 2

Entry	Decene ¹ (ml/min)	Ph ₃ P ¹ (ml/min)	$\frac{\mathbf{O}_{2}}{\mathbf{O}_{3}}^{1}$ (ml/min)	Coil (ml)	Nonanal ²	Nonanoic Acid ²	Decene ²
1	0.30 (1.0)	0.40 (2.0)	25 (1.50)	2	1.0	0.13	ND
2	0.36 (1.0)	0.48 (2.0)	25 (1.25)	2	1.0	0.04	ND
3	0.72 (1.0)	1.44 (2.5)	50 (1.25)	2	1.0	0.02	ND

All runs carried out at -10 °C. 1. Equivalents shown in brackets; 2. GC ratios referenced to nonanal.

A larger scale run was carried out at 13 mmol/hr and achieved a good yield of 75 % of this difficult to isolate aldehyde (Scheme 3).

Scheme 3

Decene: Ph₃P: Ozone: O2 Pressure **Reaction Coil** Throughput

comparable (Scheme 4).

Scheme 4

6.5 mmol

Other quench reagents were also evaluated these included DMS, thiodipropionic acid, Zn/AcOH and N-methylmorpholine-N-oxide, but none were as efficient as triphenylphosphine for a fully "in flow" process.

Conclusions

- reactor in a highly configurable fashion.
- comparable at 13 mmol/hr.

Future work

Acknowledgements

Funding: (gsk)



Triphenylphosphine is a stronger reducing agent than triethylphosphite and it was able to furnish the desired nonanal with a good selectivity of >10:1 (Table 2).

1. 1.31 eq. O ₃ /O ₂ , -10 °C	O II
2. 2.0 eq. Ph_3P , -10 °C H_3C	
EtOAc	(75 %)
0.2 M in EtOAc (1.08 ml/min)	
0.3 M in EtOAc (1.44 ml/min)	
206 g/Nm ³ (66 ml/min)	
1.299 +/- 0.005 bar abs.	
2ml (-10 °C)	
1.8 g/hr (13.0 mmol/hr) 30 min run.	

This result was compared to an equivalent batch experiment and was found to be

1. 1.2 eq. O ₃ /O ₂ , 30 min	O II
2. 2.0 eq. Ph ₃ P, 10 min	H ₃ C
EtOAc, -10 °C	(79 %)

• An ozoniser and analyser were successfully interfaced with a Vapourtec R4 flow

• For 1-decene ozonolysis, several quench reagents were analysed and only triphenylphosphine was deemed efficient in non-participating solvents.

• A large scale flow run was compared to an equivalent batch run and found to be

• Broaden scope to include a fully reductive quench to furnish alcohols.

• The ozoniser is capable of generating ozone at levels over two orders of magnitude higher and therefore could be coupled with larger flow technology.

• Utilise the accuracy of ozone delivery and fast reaction/quench times possible to explore the selective ozonolysis of multifunctional substrates.

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